- HIGH VOLTAGE CAPABILITY
- U.L. RECOGNISED ISOWATT218 PACKAGE (U.L. FILE \# E81734 (N)).


## APPLICATIONS:

- HORIZONTAL DEFLECTION FOR COLOUR TV AND MONITORS
- SWITCH MODE POWER SUPPLIES


## DESCRIPTION

The BUH515 is manufactured using Multiepitaxial Mesa technology for cost-effective high performance and uses a Hollow Emitter structure to enhance switching speeds.
The BUH series is designed for use in horizontal deflection circuits in televisions and monitors.


ISOWATT218

## INTERNAL SCHEMATIC DIAGRAM



## ABSOLUTE MAXIMUM RATINGS

| Symbol | Parameter | Value | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\text {CBO }}$ | Collector-Base Voltage $\left(\mathrm{I}_{\mathrm{E}}=0\right)$ | 1500 | V |
| $\mathrm{~V}_{\mathrm{CEO}}$ | Collector-Emitter Voltage $\left(\mathrm{I}_{\mathrm{B}}=0\right)$ | 700 | V |
| $\mathrm{~V}_{\text {EBO }}$ | Emitter-Base Voltage $\left(\mathrm{I}_{\mathrm{C}}=0\right)$ | 10 | V |
| $\mathrm{I}_{\mathrm{C}}$ | Collector Current | 8 | A |
| $\mathrm{I}_{\mathrm{CM}}$ | Collector Peak Current $\left(\mathrm{t}_{\mathrm{p}}<5 \mathrm{~ms}\right)$ | 12 | A |
| $\mathrm{I}_{\mathrm{B}}$ | Base Current | 5 | A |
| $\mathrm{I}_{\mathrm{B}}$ | Base Peak Current $\left(\mathrm{t}_{\mathrm{p}}<5 \mathrm{~ms}\right)$ | 8 | A |
| $\mathrm{P}_{\text {tot }}$ | Total Dissipation at $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$ | 50 | W |
| $\mathrm{~T}_{\text {stg }}$ | Storage Temperature | -65 to 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{j}}$ | Max. Operating Junction Temperature | 150 | ${ }^{\circ} \mathrm{C}$ |

THERMAL DATA

| $R_{\text {thj-case }}$ | Thermal Resistance Junction-case | Max | 2.5 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| :--- | :--- | :--- | :--- | :--- |

ELECTRICAL CHARACTERISTICS ( $\mathrm{T}_{\text {case }}=25^{\circ} \mathrm{C}$ unless otherwise specified)

| Symbol | Parameter | Test Conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ICES | Collector Cut-off Current ( V BE $=0$ ) | $\begin{array}{ll} \hline \mathrm{V}_{C E}=1500 \mathrm{~V} & \\ \mathrm{~V}_{C E}=1500 \mathrm{~V} & \mathrm{~T}_{\mathrm{j}}=125^{\circ} \mathrm{C} \end{array}$ |  |  | $\begin{gathered} 0.2 \\ 2 \end{gathered}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| $\mathrm{I}_{\text {ebo }}$ | Emitter Cut-off Current ( $\mathrm{IC}=0$ ) | $\mathrm{V}_{\text {Eb }}=5 \mathrm{~V}$ |  |  | 100 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {CEO(sus)* }}$ | Collector-Emitter Sustaining Voltage ( $\mathrm{IB}_{\mathrm{B}}=0$ ) | $\mathrm{IC}_{\mathrm{C}}=100 \mathrm{~mA}$ | 700 |  |  | V |
| $V_{\text {Ebo }}$ | Emitter-Base Voltage $(\mathrm{Ic}=0)$ | $\mathrm{I}_{\mathrm{E}}=10 \mathrm{~mA}$ | 10 |  |  | V |
| $\mathrm{V}_{\mathrm{CE} \text { (sat)* }}$ | Collector-Emitter Saturation Voltage | $\mathrm{I}_{\mathrm{C}}=5 \mathrm{~A} \quad \mathrm{I}_{\mathrm{B}}=1.25 \mathrm{~A}$ |  |  | 1.5 | V |
| $\mathrm{V}_{\text {be(sat) }}{ }^{*}$ | Base-Emitter Saturation Voltage | $\mathrm{I}_{\mathrm{C}}=5 \mathrm{~A} \quad \mathrm{I}_{\mathrm{B}}=1.25 \mathrm{~A}$ |  |  | 1.3 | V |
| $\mathrm{h}_{\text {FE* }}$ | DC Current Gain | $\begin{array}{lll} \hline \mathrm{I} \mathrm{C}=5 \mathrm{~A} & \mathrm{~V}_{\mathrm{CE}}=5 \mathrm{~V} & \\ \mathrm{I}_{\mathrm{C}}=5 \mathrm{~A} & \mathrm{~V}_{\mathrm{CE}}=5 \mathrm{~V} & \mathrm{~T}_{\mathrm{j}}=100^{\circ} \mathrm{C} \end{array}$ | $\begin{aligned} & 6 \\ & 4 \end{aligned}$ |  | 12 |  |
| $\begin{aligned} & \mathrm{t}_{\mathrm{s}} \\ & \mathrm{t}_{\mathrm{f}} \end{aligned}$ | RESISTIVE LOAD <br> Storage Time <br> Fall Time | $\begin{array}{ll} \mathrm{V}_{\mathrm{CC}}=400 \mathrm{~V} & \mathrm{I}_{\mathrm{C}}=5 \mathrm{~A} \\ \mathrm{I}_{\mathrm{B} 1}=1.25 \mathrm{~A} & \mathrm{I}_{\mathrm{B} 2}=2.5 \mathrm{~A} \end{array}$ |  | $\begin{aligned} & 2.7 \\ & 190 \end{aligned}$ | $\begin{aligned} & 3.9 \\ & 280 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{s} \\ & \mathrm{~ns} \end{aligned}$ |
| $\begin{aligned} & \mathrm{t}_{\mathrm{s}} \\ & \mathrm{t}_{\mathrm{f}} \end{aligned}$ | INDUCTIVE LOAD <br> Storage Time <br> Fall Time | $\begin{array}{ll} \mathrm{I}_{\mathrm{C}}=5 \mathrm{~A} & \mathrm{f}=15625 \mathrm{~Hz} \\ \mathrm{I}_{\mathrm{B} 1}=1.25 \mathrm{~A} & \mathrm{I}_{\mathrm{B} 2}=-1.5 \mathrm{~A} \\ \mathrm{~V}_{\text {ceflyback }}=1050 \sin \left(\frac{\pi}{5} 10^{6}\right) \mathrm{t} \end{array}$ |  | $\begin{aligned} & 2.3 \\ & 350 \end{aligned}$ |  | $\begin{aligned} & \mu \mathrm{s} \\ & \mathrm{~ns} \end{aligned}$ |
| $\begin{aligned} & \mathrm{t}_{\mathrm{s}} \\ & \mathrm{t}_{\mathrm{f}} \end{aligned}$ | INDUCTIVE LOAD <br> Storage Time Fall Time | $\begin{array}{ll} \hline I_{C}=5 \mathrm{~A} & f=31250 \mathrm{~Hz} \\ \mathrm{I}_{\mathrm{B} 1}=1.25 \mathrm{~A} & \mathrm{I}_{\mathrm{B} 2}=-1.5 \mathrm{~A} \\ \mathrm{~V}_{\text {ceflyback }}=1200 \sin \left(\frac{\pi}{5} 10^{6}\right) \mathrm{t} \quad \mathrm{~V} \end{array}$ |  | $\begin{aligned} & 2.3 \\ & 200 \end{aligned}$ |  | $\begin{aligned} & \mu \mathrm{s} \\ & \mathrm{~ns} \end{aligned}$ |

* Pulsed: Pulse duration = $300 \mu \mathrm{~s}$, duty cycle $1.5 \%$

Safe Operating Area


Thermal Impedance


## Derating Curve



Collector Emitter Saturation Voltage


Power Losses at 16 KHz


## DC Current Gain



Base Emitter Saturation Voltage


Switching Time Inductive Load at 16 KHz (see figure 2)


Power Losses at 32 KHz


Reverse Biased SOA


## BASE DRIVE INFORMATION

In order to saturate the power switch and reduce conduction losses, adequate direct base current $\mathrm{I}_{\mathrm{B} 1}$ has to be provided for the lowest gain hFE at $100{ }^{\circ} \mathrm{C}$ (line scan phase). On the other hand, negative base current $\mathrm{I}_{\mathrm{B} 2}$ must be provided to turn off the power transistor (retrace phase).
Most of the dissipation, in the deflection application, occurs at switch-off. Therefore it is essential to determine the value of $\mathrm{I}_{\mathrm{B} 2}$ which minimizes power losses, fall time $\mathrm{tf}_{f}$ and, consequently, $\mathrm{T}_{\mathrm{j}}$. A new set of curves have been defined to give total power losses, $\mathrm{t}_{\mathrm{s}}$ and $\mathrm{t}_{\mathrm{f}}$ as a function of lB2 at both 16 KHz and 32 KHz scanning frequencies for choosing the optimum negative drive. The test circuit is illustrated in

Switching Time Inductive Load at 32 KHz (see figure 2)


Switching Time Resistive Load

figure 1.
Inductance $L_{1}$ serves to control the slope of the negative base current lB2 to recombine the excess carrier in the collector when base current is still present, this would avoid any tailing phenomenon in the collector current.
The values of $L$ and $C$ are calculated from the following equations:
$\frac{1}{2} L(I C)^{2}=\frac{1}{2} C\left(V_{C E f l y}\right)^{2}$
$\omega=2 \pi f=\frac{1}{\sqrt{L C}}$
Where $\mathrm{I}_{\mathrm{C}}=$ operating collector current, $\mathrm{V}_{\text {CEfly }}=$ flyback voltage, $f=$ frequency of oscillation during retrace.

Figure 1: Inductive Load Switching Test Circuits.


Figure 2: Switching Waveforms in a Deflection Circuit


| DIM. | mm |  |  | inch |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN. | TYP. | MAX. | MIN. | TYP. | MAX. |
| A | 5.35 |  | 5.65 | 0.211 |  | 0.222 |
| C | 3.30 |  | 3.80 | 0.130 |  | 0.150 |
| D | 2.90 |  | 3.10 | 0.114 |  | 0.122 |
| D1 | 1.88 |  | 2.08 | 0.074 |  | 0.082 |
| E | 0.75 |  | 0.95 | 0.030 |  | 0.037 |
| F | 1.05 |  | 1.25 | 0.041 |  | 0.049 |
| F2 | 1.50 |  | 1.70 | 0.059 |  | 0.067 |
| F3 | 1.90 |  | 2.10 | 0.075 |  | 0.083 |
| G | 10.80 |  | 11.20 | 0.425 |  | 0.441 |
| H | 15.80 |  | 16.20 | 0.622 |  | 0.638 |
| L |  |  |  |  | 0.354 |  |
| L1 | 20.80 |  | 21.20 | 0.819 |  | 0.835 |
| L2 | 19.10 |  | 19.90 | 0.752 |  | 0.783 |
| L3 | 22.80 |  | 23.60 | 0.898 |  | 0.929 |
| L4 | 40.50 |  | 42.50 | 1.594 |  | 1.673 |
| L5 | 4.85 |  | 5.25 | 0.191 |  | 0.207 |
| L6 | 20.25 |  | 20.75 | 0.797 |  | 0.817 |
| N | 2.1 |  | 2.3 | 0.083 |  | 0.091 |
| R |  |  |  |  | 0.181 |  |
| DIA | 3.5 |  | 3.7 | 0.138 |  | 0.146 |



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